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Casimir effect across a layered medium

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Using nonstandard recursion relations for Fresnel coefficients involving successive stacks of layers, we extend the Lifshitz formula to configurations with an inhomogeneous, n -layered, medium separating two planar objects. The force on each object is the sum of a Lifshitz like force and a force arising from the inhomogeneity of the medium. The theory correctly reproduces very recently obtained results for the Casimir force/energy in some simple systems of this kind. As a by product, we obtain a formula for the force on an (unspecified) stack of layers between two planar objects which generalizes our previous result for the force on a slab in a planar cavity.

Keywords: Casimir force; Fresnel coefficients; nonstandard recursion.

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1. Introduction

Very recently, several papers appeared dealing with the theory of the Casimir effect in systems consisting of two perfectly reflecting plates separated by a layered medium^{1,2,3}. Among the other results, these works provided formulas for the Casimir force and/or energy for a few simple systems of this sort (with up to five layers media¹ between the plates). Using the theory of the Casimir effect in multilayers⁴ and nonstandard recursion relations for Fresnel coefficients^{4,5,6,7}, in this Note we derive formulas for the Casimir force and energy for systems with arbitrary plates separated by arbitrary inhomogeneous, generally n -layered, media.

2. Casimir effect across a layered medium

Consider the system consisting of two planar objects (plates) separated by a layered medium, as depicted in Fig. 1. According to the theory of the Casimir effect in multilayers⁴, the Casimir forces on the left (L) and the right (R) plate are given by

$$F_L \equiv F_{1-} = T_{zz}^{(1)} \quad \text{and} \quad F_R \equiv F_{n+} = -T_{zz}^{(n)}, \quad (1)$$

respectively, where (unless necessary, we omit the polarization index $q = p, s$ when writing Fresnel coefficients)

$$T_{zz}^{(j)} = \frac{\hbar}{2\pi^2} \int_0^\infty d\xi \int_0^\infty dk k \kappa_j \sum_q \frac{r_{j-} r_{j+} e^{-2\kappa_j d_j}}{1 - r_{j-} r_{j+} e^{-2\kappa_j d_j}} \quad (2)$$

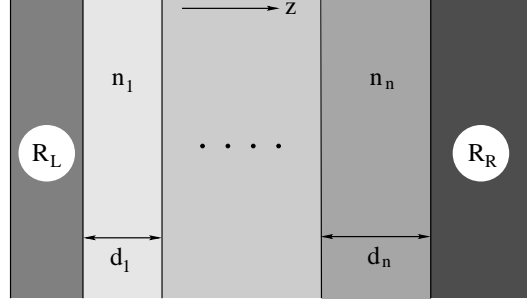


Fig. 1. Two plates separated by a layered medium shown schematically. Plates are described by their reflection coefficients R_L and R_R and the medium layers by their (complex) refraction indexes $n_a(\omega) = \sqrt{\varepsilon_a(\omega)\mu_a(\omega)}$, $a = 1 \dots n$.

is the relevant component of the vacuum-field (Minkowski) stress tensor in the layer j . Here $\kappa_j = \sqrt{n_j^2(i\xi)\xi^2/c^2 + k^2}$ is the perpendicular wave vector at the imaginary frequency ($\omega = i\xi$) in the layer, $k = \sqrt{k_x^2 + k_y^2}$ is the magnitude of the wave vector parallel to the system surfaces and $r_{j\pm}(i\xi, k)$ are the reflection coefficients of the right and left stack of layers bounding the layer j . These reflection coefficients obey generalized recursion relations^{4,5,6,7}

$$r_{j\pm} = r_{j/l} + \frac{t_{j/l}t_{l/j}r_{l\pm}e^{-2\kappa_l d_l}}{1 - r_{l/j}r_{l\pm}e^{-2\kappa_l d_l}}, \quad t_{j\pm} = \frac{t_{j/l}t_{l\pm}e^{-\kappa_l d_l}}{1 - r_{l/j}r_{l\pm}e^{-2\kappa_l d_l}}, \quad (3)$$

where l denotes an intermediate layer and where the symbol $a/b \equiv a \dots b$ is used to denote the stack of layers between layers a and b . As seen, these recurrence relations look the same as the standard ones^{8,9} (to which they reduce in case that layers j and l are neighbor layers), however, this time they generally involve Fresnel coefficients $r_{j/l}$, $r_{l/j}$, $t_{j/l}$ and $t_{l/j}$ of the *stack* between the layers j and l .

Using the above recursion relations, reflection coefficients r_{1+} and r_{n-} can be expressed as

$$r_{1+} = \frac{r_{1/n} + a_{1/n}R_R e^{-2\kappa_n d_n}}{1 - r_{n/1}R_R e^{-2\kappa_n d_n}}, \quad r_{n-} = \frac{r_{n/1} + a_{n/1}R_L e^{-2\kappa_1 d_1}}{1 - r_{1/n}R_L e^{-2\kappa_1 d_1}}, \quad (4)$$

where we have introduced the quantity

$$a_{1/n} = t_{1/n}t_{n/1} - r_{1/n}r_{n/1} = a_{n/1} \quad (5)$$

and identified r_{n+} and r_{1-} as the reflection coefficients R_R and R_L , respectively, of the plates. Therefore, from (1) and (2) we obtain for the forces on the plates

$$F_L = \frac{\hbar}{2\pi^2} \int_0^\infty d\xi \int_0^\infty dk k \kappa_1 \sum_q \frac{1}{N_n} (r_{1/n} + a_{1/n}R_R e^{-2\kappa_n d_n}) R_L e^{-2\kappa_1 d_1}, \quad (6a)$$

$$F_R = \frac{-\hbar}{2\pi^2} \int_0^\infty d\xi \int_0^\infty dk k \kappa_n \sum_q \frac{1}{N_n} (r_{n/1} + a_{n/1}R_L e^{-2\kappa_1 d_1}) R_R e^{-2\kappa_n d_n}, \quad (6b)$$

where

$$N_n = 1 - (r_{1/n} R_L e^{-2\kappa_1 d_1} + r_{n/1} R_R e^{-2\kappa_n d_n}) - a_{1/n} R_L R_R e^{-2\kappa_1 d_1 - 2\kappa_n d_n}. \quad (7)$$

As seen, since $r_{1/n} \neq r_{n/1}$ unless the medium is not symmetric across the gap, these forces are not generally equal in magnitude and each of them consists of a Lifshitz-like force (given by the second terms in (6)) and a force due to the inhomogeneity of the medium. We also note that owing to the medium inhomogeneity there is a force⁴ $F_S = T_{zz}^{(n)} - T_{zz}^{(1)} = -F_R - F_L$ on the central stack of the medium given explicitly by

$$F_S = \frac{\hbar}{2\pi^2} \int_0^\infty d\xi \int_0^\infty dk k \sum_q \frac{1}{N_n} (\kappa_n r_{n/1} R_R e^{-2\kappa_n d_n} - \kappa_1 r_{1/n} R_L e^{-2\kappa_1 d_1}) + (\kappa_n - \kappa_1) \frac{a_{1/n}}{N_n} R_L R_R e^{-2\kappa_1 d_1 - 2\kappa_n d_n}. \quad (8)$$

When $n_1 = n_n$, this generalizes previously obtained result for the force on a slab in a planar cavity^{4,7,10} to configurations with the slab replaced by an unspecified multilayered stack.

Having determined forces on the plates, we can calculate the Casimir energy of the system from⁴ $F_L = \partial E / \partial d_1$ or $F_R = -\partial E / \partial d_n$. We obtain

$$E = \frac{\hbar}{(2\pi)^2} \int_0^\infty d\xi \int_0^\infty dk k \sum_q \ln N_n. \quad (9)$$

In the following, we illustrate this formula by discussing its implications for several simple systems and comparing them with the results obtained in Refs. 1-3.

3. Discussion

It is easy to see that (7) and (9) give correctly the Casimir energy in case of a homogeneous medium between the plates. Indeed, assuming that all n medium layers are made of the same matter ($n_a = n$, $\kappa_a = \kappa$), we have $r_{1/n} = r_{n/1} = 0$ and $t_{1/n} = t_{n/1} = \exp[-\kappa(d - d_1 - d_n)]$ so that $a_{1/n} = \exp[-2\kappa(d - d_1 - d_n)]$ and

$$N_n = 1 - R_L R_R e^{-2\kappa d}, \quad (10)$$

where d is the distance between the plates. This leads to the standard Lifshitz-type formula¹¹ for the Casimir energy. For perfectly reflecting plates^{2,3}, we must let here $R_L R_R = 1$.

In the $n = 2$ case (two media between the plates), we have $r_{1/2} = r_{12} = -r_{21} = -r_{2/1}$ and $t_{1/2} = t_{12} = (\mu_2 \kappa_1 / \mu_1 \kappa_2) t_{21} = (\mu_2 \kappa_1 / \mu_1 \kappa_2) t_{2/1}$, where r_{12} and t_{12} are the *single-interface* Fresnel coefficients^{4,5}

$$r_{12} = \frac{\kappa_1 - \gamma_{12} \kappa_2}{\kappa_1 + \gamma_{12} \kappa_2} = -r_{21}, \quad t_{12} = \sqrt{\frac{\gamma_{12}}{\gamma_{12}^s}} (1 + r_{12}) = \frac{\mu_2 \kappa_1}{\mu_1 \kappa_2} t_{21}, \quad (11)$$

with $\gamma_{12}^p = \varepsilon_1 / \varepsilon_2$ and $\gamma_{12}^s = \mu_1 / \mu_2$. Noting that $a_{1/2} = 1$, we have

$$N_2 = 1 - r_{12} (R_L e^{-2\kappa_1 d_1} - R_R e^{-2\kappa_2 d_2}) - R_L R_R e^{-2(\kappa_1 d_1 + \kappa_2 d_2)}, \quad (12)$$

which, in conjunction with (9), gives the Casimir energy for the present system. This result coincides with the corresponding result obtained in Ref. 2 providing that we let for perfectly reflecting plates $R_{L(R)}^q = -1$. We note, however, that perfect reflectors are standardly simulated by media with infinitely large permittivities (conductivities) in which case (11) implies ($\varepsilon_2 \rightarrow \infty$) that $R_{L(R)}^s = -1$ but $R_{L(R)}^p = 1$. Therefore, with this convention, our result disagrees with that of Ref. 2 regarding the p contribution to the Casimir force/energy.

Using recursion relations (3), E for more complex ($n \geq 3$) systems can be written in terms of lower-layered stacks and, owing to the number of the medium layers, this can be done in a number of ways. Clearly, to obtain the effective Casimir energy, we can drop from these results the terms not involving d_1 or d_n . Thus, for example, from (3) we have⁷

$$r_{1/n} = \frac{r_{1/l} + a_{1/l}r_{l/n}e^{-2\kappa_l d_l}}{D_l}, \quad r_{n/1} = \frac{r_{n/l} + a_{n/l}r_{l/1}e^{-2\kappa_l d_l}}{D_l}, \quad (13a)$$

$$a_{1/n} = \frac{a_{1/l}a_{n/l}e^{-2\kappa_l d_l} - r_{1/l}r_{n/l}}{D_l}, \quad D_l = 1 - r_{l/1}r_{l/n}e^{-2\kappa_l d_l}. \quad (13b)$$

Using this in (7) and rearranging, we find

$$N_n = \frac{N_n^{(l)}}{D_l}, \quad (14)$$

where

$$N_n^{(l)} = (1 - r_{1/l}R_L e^{-2\kappa_1 d_1})(1 - r_{n/l}R_R e^{-2\kappa_n d_n}) - e^{-2\kappa_l d_l}(a_{1/l}R_L e^{-2\kappa_1 d_1} + r_{l/1})(a_{n/l}R_R e^{-2\kappa_n d_n} + r_{l/n}). \quad (15)$$

Finally, inserting this N_n in (9) and dropping the (ineffective) term involving D_l , we find for the effective Casimir energy E_l of the system (with respect to the layer l)

$$E_l = \frac{\hbar}{(2\pi)^2} \int_0^\infty d\xi \int_0^\infty dk k \sum_q \ln N_n^{(l)}. \quad (16)$$

This generalizes the ($T = 0$) result for the Casimir interaction energy between two slabs obtained in Ref 1 using a realistic Casimir piston approach and a five layer model for the medium to arbitrary multilayered slabs and plates. Note that, when removing the plates by letting $d_{1(n)} \rightarrow \infty$, we have $N_n^{(l)} \rightarrow D_l$ and (15) and (16) give the Casimir interaction energy of the two stacks of layers separated by a layer of medium l , as derived in Ref. 4.

We illustrate the above result by considering the $n=3$ system. In this case, there is only one intermediate layer and the effective Casimir energy (16) is entirely expressed in terms of the single-interface reflection coefficients $r_{12} = -r_{21}$ and $r_{32} = -r_{23}$. From (15), we have ($a_{1/2} = a_{3/2} = 1$)

$$N_3^{(2)} = (1 - r_{12}R_L e^{-2\kappa_1 d_1})(1 - r_{32}R_R e^{-2\kappa_3 d_3}) - e^{-2\kappa_2 d_2}(R_L e^{-2\kappa_1 d_1} - r_{12})(R_R e^{-2\kappa_3 d_3} - r_{32}). \quad (17)$$

As mentioned, for perfectly reflecting plates we must let here $R_{L(R)}^q = \delta_{qp} - \delta_{qs}$. This result then coincides with the corresponding result derived in Ref. 1 whereas the results obtained in Refs. 2 and 3 correspond to plates with $R_{L(R)}^q = -1$ and $R_{L(R)}^q = 1$, respectively.

4. Summary

Effectively, in this work we have extended the Lifshitz formula to configurations with an inhomogeneous, n-layered, medium separating two planar objects. The force on each object is the sum of a Lifshitz-like force and a force arising from the inhomogeneity of the medium. Owing to this inhomogeneity, there is also a force acting on the medium. When the first and the last medium layer are made of the same matter, this result generalizes previously obtained one for the force on a slab in a planar cavity to arbitrary multilayered slabs.

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